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FOURTH PROGRESS REPORT
FOR
RESEARCH INTO FUNDAMENTAL PHENOMENA ASSOCIATED WITH SPACECRAFT
ELECTROCHEMICAL DEVICES — CALORIMETRY OF NICKEL-CADMIUM
CELLS

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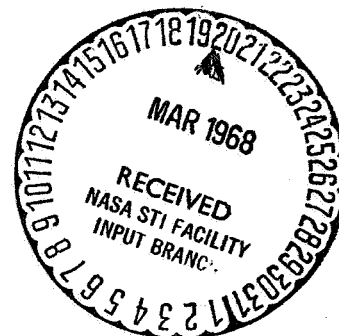


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ABSTRACT

The present work on this project consists of calorimetric measurements on nickel-cadmium cells of various capacities undergoing discharge at depths of 15, 25, and 40%, and recharge at 110%.

During this reporting period changes were made in the system to accommodate the larger 20 ampere-hour cell and to increase the reproducibility and sensitivity of the heat measurement. These changes included rebuilding the external heat exchanger, altering the flow pattern of the oil through the calorimeter, and fabricating an improved thermopile.

Calibration experiments on the heater and the pressure transducer were performed.

The data from the charge efficiency study on the six ampere-hour cell reported in the Second Progress Report were replotted to better represent the heat dissipation problem.

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I. INTRODUCTION

During the period following the Third Progress Report several changes in the overall system were made. These changes were made necessary when the system was adapted for the twenty ampere-hour nickel-cadmium cell and, subsequently, to achieve greater reproducibility and sensitivity in measuring the heat output on calibration.

These changes included rebuilding the heat exchanger in the constant temperature bath external to the calorimeter, altering the flow pattern of the oil through the calorimeter, and fabricating an improved thermopile. Following these changes calibration experiments were performed on the heater and the pressure transducer.

The charge efficiency study on the six ampere-hour nickel-cadmium cell was reported in the Second Progress Report of this series. These data have been plotted and presented in a form more readily comprehended.

In a final paragraph the work contemplated for future reporting periods is outlined.

II. DESIGN AND FABRICATION CHANGES IN THE SYSTEM

The design and construction of a new and larger calorimeter, as reported in the Third Progress Report, has been accompanied by several improvements and modifications. The areas in which these improvements were made were both in the internal and external systems. The external improvement consisted of replacing the heat exchanger in the Aminco constant temperature bath. The internal improvements were a) a change in the flow system, b) the construction of a new thermopile, and c) a change in the calibration heater on the cell fixture. A general view of the present apparatus is shown in Figure 1.

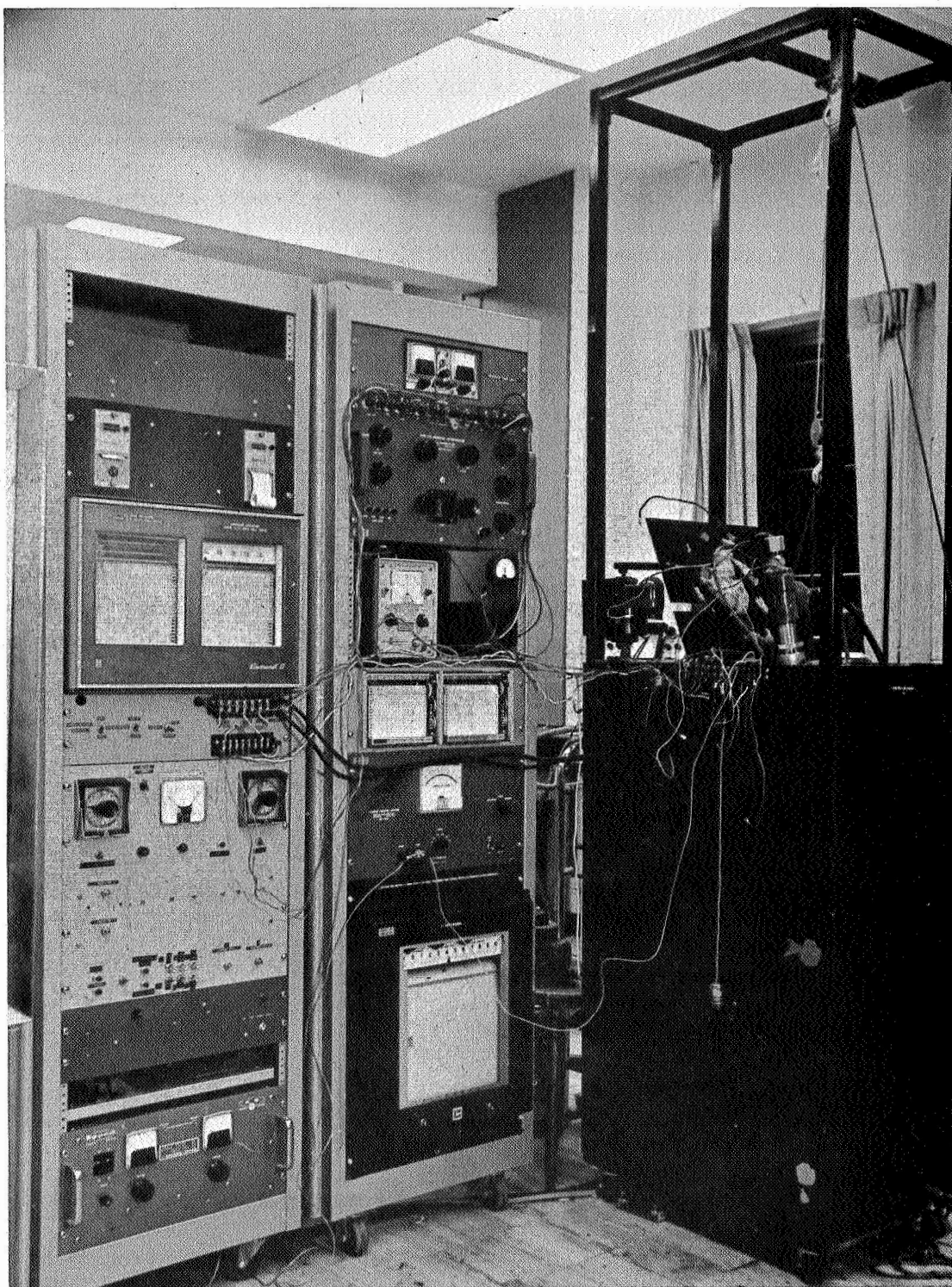


Figure 1. General view of Continuous-Flow Calorimeter and Associated Electrical Equipment

The Heat Exchanger

The construction of a new heat exchanger in the Aminco constant temperature bath was intended to minimize environmental heat effects and to increase the isothermal nature of the calorimetric system. The original heat exchanger, described in the First Progress report was constructed of straight copper tubing. The new exchanger was constructed with aluminum-finned-copper tubing. Twenty inch sections of the 0.75 in. diameter copper tubing were fitted with the appropriate copper elbows and soldered together to make a unit of 13 feet total length. This has improved the stability of the thermostat system.

The Flow System

To further increase the control of environmental effects the flow pattern of the oil was altered. In the previous system the on-off cycling of the refrigeration unit in the Aminco constant temperature bath would appear as a ripple on the chart recording the thermopile output. In the original arrangement, as described in the First Progress Report, the oil was forced from the external constant temperature bath into the calorimeter proper. Such an arrangement did not allow for proper equilibration of the oil and this showed up as a disturbing ripple in the thermopile reading. The new flow pattern for the oil is shown in Figure 2. The modified flow system draws the oil into the calorimeter from the bottom of the tank. The oil passes the cold junction of the thermopile, circulates around the heater and the cell itself, and then passes over the hot junction of the thermopile. Above the hot junction there is a rubber hose connected to the neck of the calorimeter and leading to the metering pump. The oil is drawn through the calorimeter,

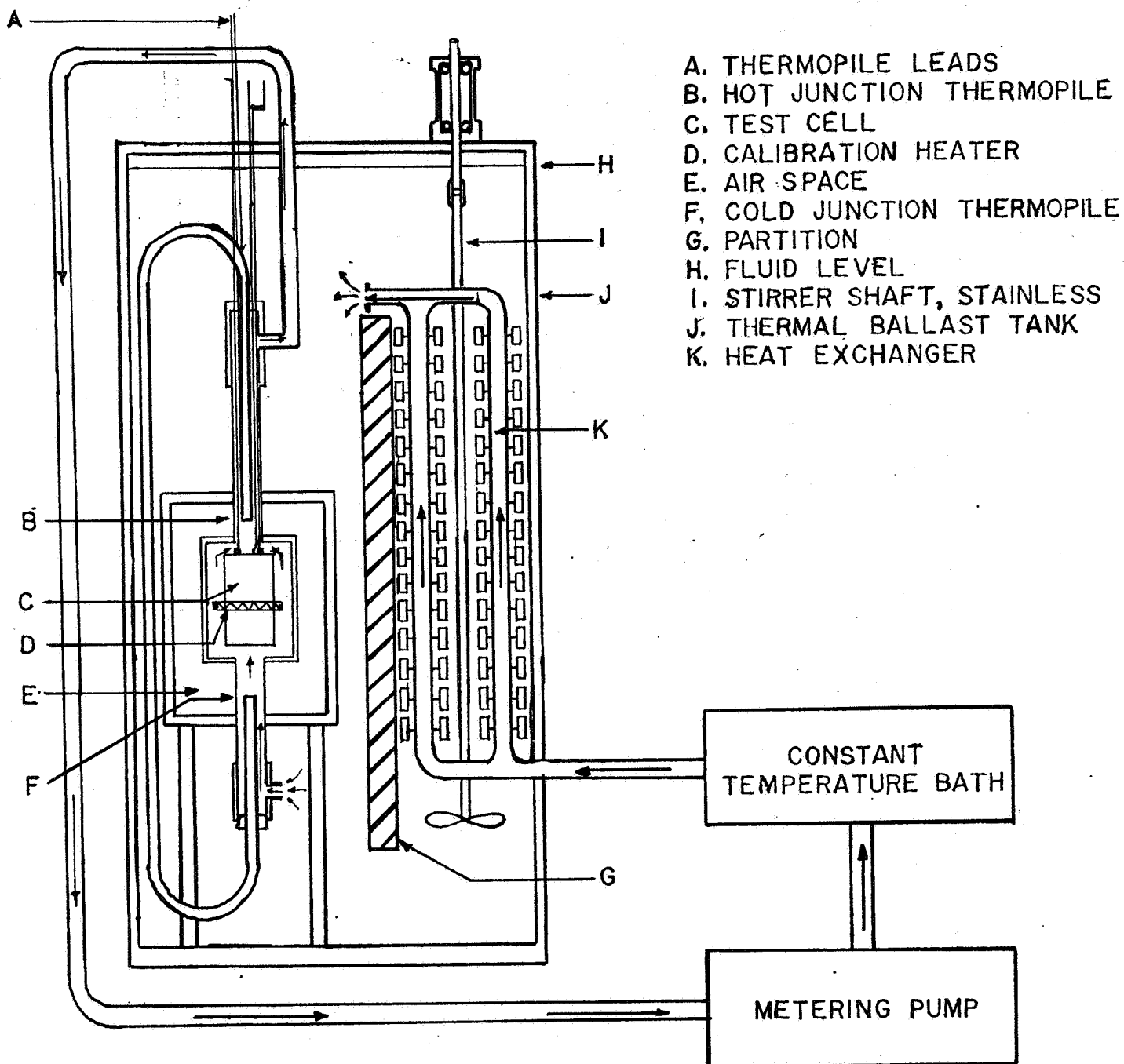


Figure 2. Flow pattern of oil through calorimeter, pump, constant temperature bath and heat exchangers

in the manner described above, into the metering pump which pumps it through the new heat exchanger, and then through the copper-finned internal heat exchanger before depositing it into the thermal ballast tank. The flow described above allows the calorimeter to take in oil from a constant temperature reservoir rather than from the constant temperature bath, thus eliminating the cycling effect of the bath on the signal output of the heat recorder.

The Thermopile

The third change made was the construction of a new and more sensitive thermopile. The new twenty-five junction copper-constantan thermopile was constructed to eliminate the use of bulky solder joints and Teflon tubing. The previously constructed thermopile was described in the First Progress Report, page 34, and Fig. 8. In principle the system has not been changed. The modifications made have been in the construction of the thermopile itself. The improvements in the thermopile are as follows: (1) the copper-constantan junctions were spot welded; (2) the leads were mounted on a Teflon support (1.00 inch in length and 0.625 inch in diameter). Therefore the Teflon tubing, the Armstrong Epoxy cement and the solder have all been eliminated. The new Teflon support was machined in such a way that each lead going into making the junction would be shielded to prevent shorting from one junction to another. Aside from the obvious advantages of eliminating the Teflon tubing, the epoxy cement and the bulky solder joints, the overall advantage is greater response and increased thermal sensitivity. This construction is schematically shown in Figure 3.

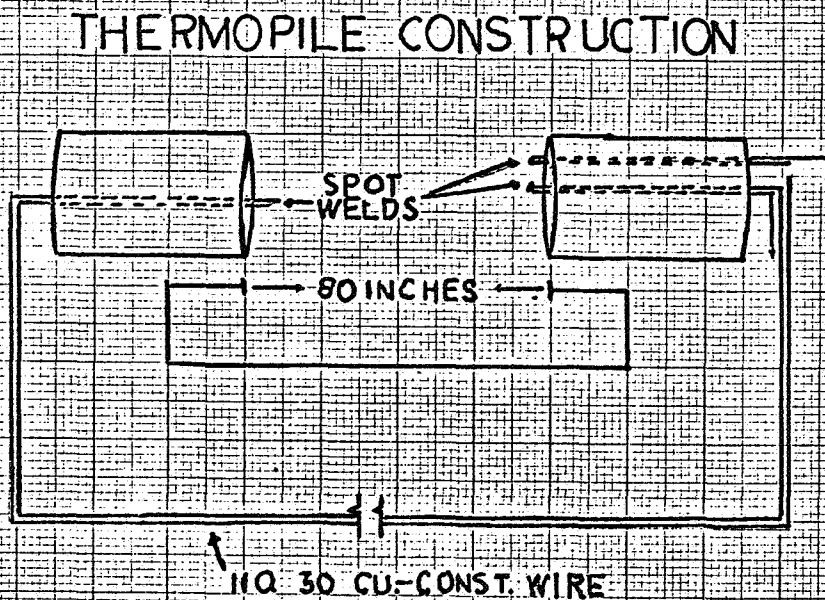
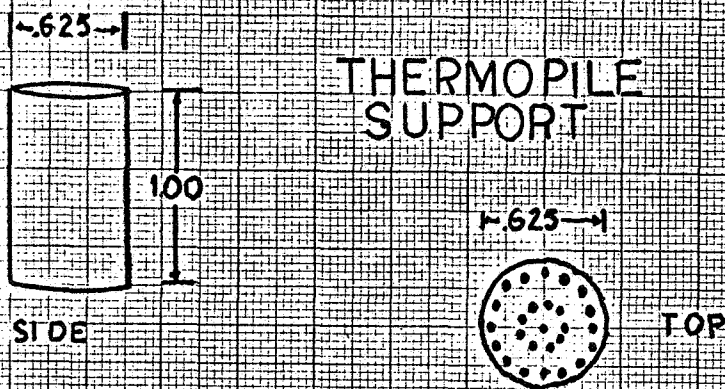


Figure 3. Thermopile construction

The Calibration Heater

In order to allow for the larger size of the 20-AH nickel-cadmium cell as compared with the 6-AH cell a modification of the Lucite fixture supporting the unit was required. From the diagram of the flow system (Fig. 2) it will be observed that the distance between the calibration heater and the lower (cold) junction of the thermopile is critical. Whereas the heater should approximate, in a geometrical way, the heat given off by the cell, it must be positioned within the limits of the critical distance. To have the calibration heater uniformly heat the system the fixture was redesigned so that the resistance heater was located 1/2 inch from the cell on both sides of the cell. Previously the heater was located under the cell, but the same distance from the lower end of the Lucite fixture. The advantages of this rearrangement are twofold: (1) it does not interfere with the positioning of the cell; (2) more heat is put into the system and less heat or no heat goes into heating the bottom end of the cell.

III. CALIBRATION STUDIES

Heater Calibration

In order to calibrate the newly constructed thermopile, the calorimeter was fitted with a calibration heater as described above. The procedure for making the calibration consisted of the following steps: (1) with the cell in place and the calorimeter ready to be operated a heat versus flow rate profile was established. From the results so obtained the flow rate corresponding to a maximum signal output from the thermopile was obtained; (2) the resistance of the heater was next determined; (3) the current input to give the desired voltage was then calculated; (4)

the microvolt signal of the thermopile versus the voltage over the desired calibration range was recorded.

A series of calibrations is given in Table 1. The plot of watts versus microvolt output for a pumping rate corresponding to 45% stroke rate of the metering pump is given in Figure 4. The 45% stroke rate corresponds to a flow rate of approximately 2500 cc/minute and was obtained by the step one procedure. The resistance of the heater was 0.426 ohms (an average of several measurements). This calibration curve was carried to about 5 watts output which covered the range of output for the 20 ampere-hour cell under the conditions of the planned experiment.

Pressure Transducer Calibration

The 20 ampere-hour cell was fitted with a Glennite pressure transducer to monitor the oxygen pressure in the cell and also to check and interpret the readings observed from the third electrode. A preliminary calibration value for Glennite transducer #101 measured at the Goddard Space Flight Center was 400 millivolts, equivalent to 150 psia under an operating voltage of 8.85 v. The output of this transducer at a number of pressure values was measured. During these tests the cell was filled with a known oxygen pressure as determined by a mercury barometer. The output of the transducer was plotted against the actual oxygen pressure in Figure 5. The so-called "indicated psia" is taken from the linear relationship based on $400 \text{ mv} = 150 \text{ psia}$.

IV. CHARGE EFFICIENCY OF THE SIX AMPERE-HOUR CELL

The charge efficiency study carried out on a Gulton 6 ampere-hour cell was reported in part in the Second Progress Report (pp. 3, 11-15). To give a more complete picture of the cell's efficiency at the various

*Data in table 2.

Table 1. Heater Calibration Data

45% Stroke,
Heater Resistance = 0.426 ohms

| <u>Signal (μv)</u> | <u>Heat (watts)</u> |
|-----------------------------------|---------------------|
| -6 | 0.0 |
| 36 | 0.5 |
| 79 | 1.0 |
| 121 | 1.5 |
| 165 | 2.0 |
| 208 | 2.5 |
| 250 | 3.0 |
| 292 | 3.5 |
| 336 | 4.0 |
| 380 | 4.5 |

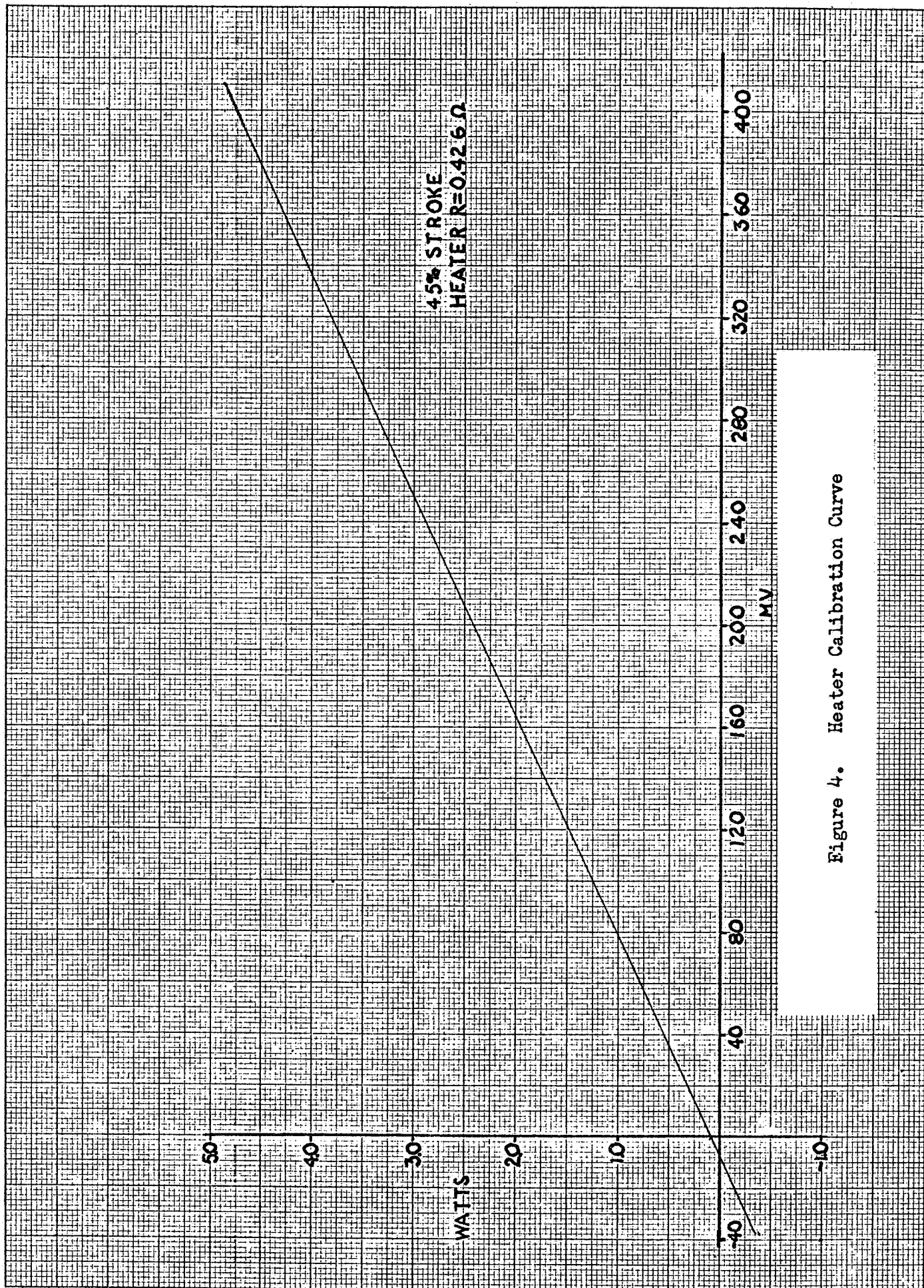


Figure 4. Heater Calibration Curve

Table 2. Pressure Transducer Calibration Data

| <u>Signal (μv)</u> | <u>Pressure</u> | |
|-----------------------------------|---------------------------|------------------------|
| | <u>Indicated P.S.I.A.</u> | <u>Actual P.S.I.A.</u> |
| 10 | 3.5 | <0 |
| 20 | 7.5 | 3.0 |
| 30 | 11 | 7.5 |
| 40 | 15 | 11.5 |
| 50 | 18.5 | 15.5 |
| 60 | 22.5 | 19.5 |
| 70 | 26 | 23.5 |
| 80 | 30 | 27.5 |
| 90 | 34 | 32.5 |
| 100 | 37.5 | 35.5 |
| 110 | 41.5 | 40 |
| 120 | 45 | 44 |
| 130 | 49 | 48 |

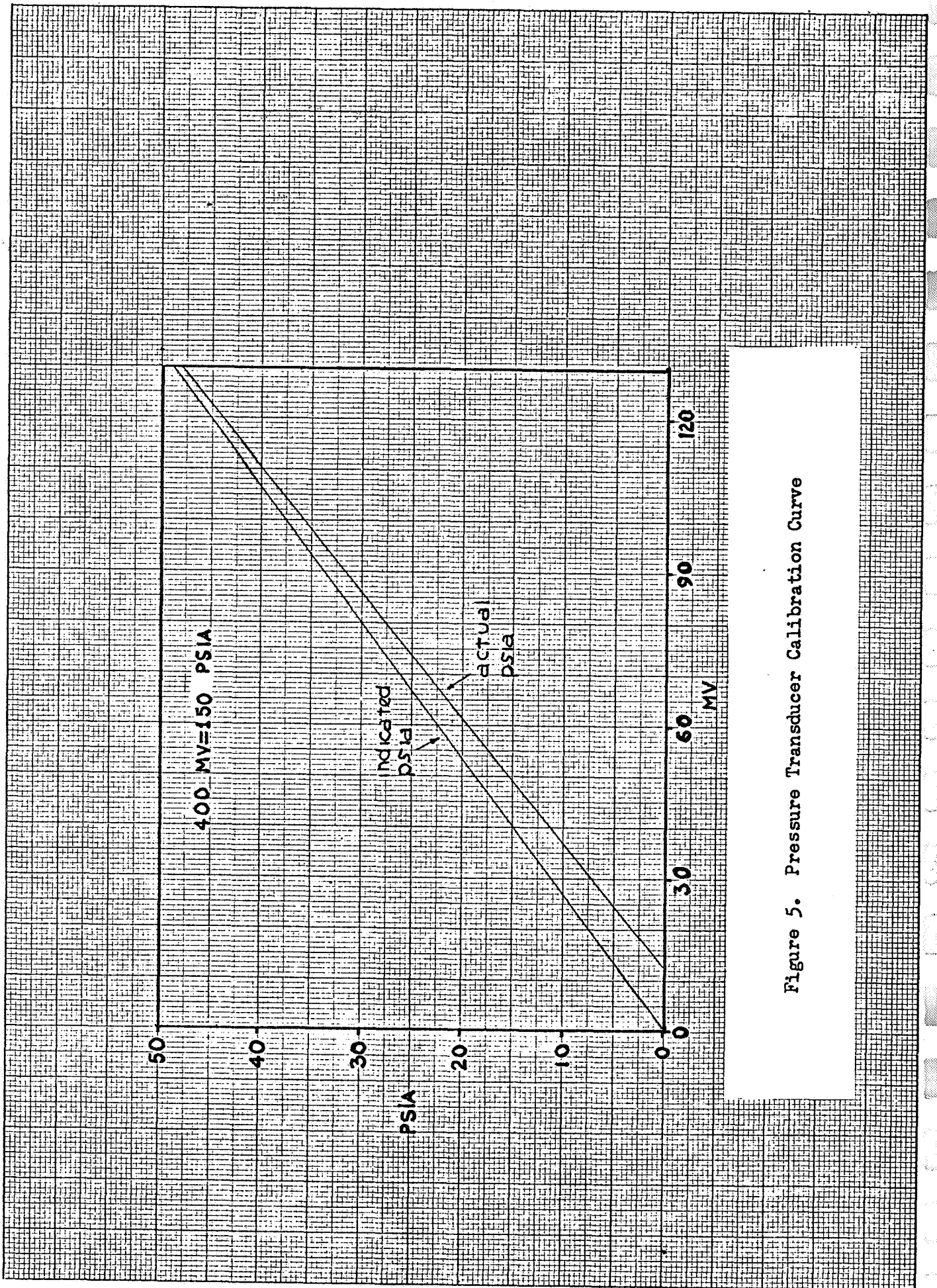


Figure 5. Pressure Transducer Calibration Curve

charging rates some of these data are plotted in Figure 6. This plot gives the heat output as a function of time. The time axis is divided into charge and discharge zones where discharge for all experiments are carried out at a C/2 rate to a voltage of 1 volt. For the charge cycle the cut-off point was taken as a signal of 100 μ v across the 6.8 ohm resistor of the third electrode. The charge rates used were C/10 (0.60 amp), C/8 (0.75 amp), C/6 (1.00 amp), C/4 (1.50 amp), C/2 (3.00 amp), and C/1.2 (5.00 amp), each at the constant indicated current. The discharge was at the 3.00 amp rate. Table 3 in the referenced report gives the results of the study in terms of cell efficiency and heat generated. Column 3 in Table 3 shows that, within the range of charging rates studied, the cell % efficiency varies by only 3.7%. The discharge process carried out at a constant current of 3.00 amps shows a constant endothermic output. Figure 6 illustrates graphically the heat dissipation problems associated with different rates of charging.

V. PLANNED FUTURE WORK

The thermal characteristics of the twenty ampere-hour cell will be evaluated at the same depths of discharge and recharge rates as those to which the six ampere-hour cell was subjected.

Figure 6. Charge Efficiency Study of Gulton 6 A-H Cell
(See Second Progress Report for Data)



TABLE 3 - Comparison of Efficiency, Charge Rate, and Thermal Response

| Charge Rate | $\frac{\text{AH Out}}{\text{AH In}}$ | % Eff. | CHARGE | | DISCHARGE |
|-----------------|--------------------------------------|--------|-------------------------------------|------------------------------------|------------------------------------|
| | | | Max. Endothermic Output(Watt) | Max. Exothermic Output(Watt) | Max. Exothermic Output(Watt) |
| $\frac{C}{1.2}$ | $\frac{6.734}{8.134}$ | 82.7 | +0.10 | -0.24 | -0.69 |
| $\frac{C}{2}$ | $\frac{6.835}{7.959}$ | 85.8 | +0.12 | -0.12 | -0.69 |
| $\frac{C}{4}$ | $\frac{6.879}{8.200}$ | 83.8 | +0.08 | -0.10 | -0.68 |
| $\frac{C}{6}$ | $\frac{6.902}{8.237}$ | 83.7 | +0.07 | -0.10 | -0.69 |
| $\frac{C}{8}$ | $\frac{6.943}{8.466}$ | 82.1 | +0.10 | -0.10 | -0.70 |
| $\frac{C}{10}$ | $\frac{6.867}{8.190}$ | 83.8 | +0.06 | -0.12 | -0.72 |

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